

DC-OPF Formulation with Price-Sensitive Demand Bids

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1 Cost and Demand Function Representations

Generator i 's total cost function:

$$\text{TC}_i(p_{Gi}) = a_i \cdot p_{Gi} + b_i \cdot p_{Gi}^2 + \text{FCost}_i \quad (1)$$

Generator i 's total variable cost function:

$$\text{TVC}_i(p_{Gi}) = a_i \cdot p_{Gi} + b_i \cdot p_{Gi}^2 \quad (2)$$

Generator i 's marginal cost function (supply offer schedule):

$$\text{MC}_i(p_{Gi}) = a_i + 2 \cdot b_i \cdot p_{Gi} \quad (3)$$

LSE j 's demand bid p_{Lj} consists of two parts: a fixed demand bid p_{Lj}^F and a price-sensitive demand bid p_{Lj}^S , i.e.,

$$p_{Lj} = p_{Lj}^F + p_{Lj}^S \quad (4)$$

LSE j 's price-sensitive demand bid function expressing maximum willingness to pay as a function of the demanded quantity p_{Lj}^S :

$$D_j(p_{Lj}^S) = c_j - 2 \cdot d_j \cdot p_{Lj}^S \quad (5)$$

The gross surplus of LSE j corresponding to its price-sensitive demand bid:¹

$$\text{GSS}_j(p_{Lj}^S) = c_j \cdot p_{Lj}^S - d_j \cdot p_{Lj}^S{}^2 \quad (6)$$

Total net surplus corresponding to price-sensitive demand bids:²

$$\text{TNSS}(\mathbf{p}_G, \mathbf{p}_L^S) = \text{GSS}(\mathbf{p}_L^S) - \text{TVC}(\mathbf{p}_G) \quad (7)$$

¹The gross surplus of LSE j corresponding to its fixed demand bid is always infinite (vertical demand curve). For this reason, the DC-OPF objective function used by the ISO to determine efficient commitment and dispatch of generation will only take into account LSE gross surplus corresponding to price-sensitive demand bids.

²Note that TNSS coincides with the usual measure for total net surplus in the absence of fixed demand bids.

where

$$\mathbf{p}_G = (p_{G1}, p_{G2}, \dots, p_{GI}) \quad (8)$$

$$\mathbf{p}_L^S = (p_{L1}^S, p_{L2}^S, \dots, p_{LJ}^S) \quad (9)$$

$$\text{GSS}(\mathbf{p}_L^S) = \sum_{j=1}^J \text{GSS}_j(p_{Lj}^S) \quad (10)$$

$$\text{TVC}(\mathbf{p}_G) = \sum_{i=1}^I \text{TVC}_i(p_{Gi}) \quad (11)$$

$$(12)$$

Total net cost function corresponding to price-sensitive demand bids:

$$\text{TNCS}(\mathbf{p}_G, \mathbf{p}_L^S) = -\text{TNSS}(\mathbf{p}_G, \mathbf{p}_L^S) \quad (13)$$

2 DC-OPF Problem in Structural Form

A commonly used representation for an hourly DC-OPF problem with price-sensitive load bids is to minimize total net costs corresponding to the price-sensitive demand (TNCS) subject to various transmission constraints. As explained at length in Sun and Tesfation (2007), it is useful to modify the objective function for this standard DC-OPF problem to include a soft penalty function for large voltage angle deviations.

The resulting modified DC-OPF problem formulation is as follows, where all endogenous and exogenous variables are defined as in Tables (1) and (2):

Minimize

$$\text{TNCS}(\mathbf{p}_G, \mathbf{p}_L^S) + \pi \left[\sum_{km \in BR} [\delta_k - \delta_m]^2 \right] \quad (14)$$

with respect to real power generation levels, real power price-sensitive loads, and voltage angles

$$p_{Gi}, \quad i = 1, \dots, I; \quad p_{Lj}^S, \quad j = 1, \dots, J; \quad \delta_k, \quad k = 1, \dots, K$$

subject to:

Real power balance constraint for each node $k = 1, \dots, K$:

$$\sum_{i \in I_k} p_{Gi} - \sum_{j \in J_k} p_{Lj} - \sum_{km \text{ or } mk \in BR} P_{km} = 0 \quad (15)$$

where

$$p_{Lj} = p_{Lj}^F + p_{Lj}^S \quad (16)$$

$$P_{km} = B_{km} [\delta_k - \delta_m] \quad (17)$$

Alternatively,

$$\sum_{i \in I_k} p_{Gi} - \sum_{j \in J_k} p_{Lj}^S - \sum_{km \text{ or } mk \in BR} P_{km} = \sum_{j \in J_k} p_{Lj}^F \quad (18)$$

Real power thermal constraint for each branch $km \in BR$:

$$|P_{km}| \leq P_{km}^U \quad (19)$$

Real power operating capacity constraints for each Generator $i = 1, \dots, I$:

$$Cap_i^L \leq p_{Gi} \leq Cap_i^U \quad (20)$$

Real power price-sensitive load constraints for each LSE $j = 1, \dots, J$:

$$SLoad_j^L \leq p_{Lj}^S \leq SLoad_j^U \quad (21)$$

Voltage angle setting at reference node 1:

$$\delta_1 = 0 \quad (22)$$

3 DC-OPF Problem in Matrix Form

3.1 General Matrix Formulation

Let δ_1 be set to zero everywhere in the DC-OPF problem presented in the previous section 2, in accordance with constraint (22). The general matrix depiction for the resulting reduced-form DC-OPF problem can then be expressed as follows:

Minimize

$$f(\mathbf{x}) = \frac{1}{2} \mathbf{x}^T \mathbf{G} \mathbf{x} + \mathbf{a}^T \mathbf{x} \quad (23)$$

with respect to

$$\mathbf{x} = [p_{G1} \quad \dots \quad p_{GI} \quad p_{L1}^S \quad \dots \quad p_{LJ}^S \quad \delta_2 \quad \dots \quad \delta_K]^T_{(I+J+K-1) \times 1}$$

subject to

$$\mathbf{C}_{\text{eq}}^T \mathbf{x} = \mathbf{b}_{\text{eq}} \quad (24)$$

$$\mathbf{C}_{\text{iq}}^T \mathbf{x} \geq \mathbf{b}_{\text{iq}} \quad (25)$$

Given this general matrix formulation, the problem is now to find the specific matrix and vector representations \mathbf{a} and \mathbf{G} for the objective function, \mathbf{C}_{eq} and \mathbf{b}_{eq} for the equality constraints, and \mathbf{C}_{iq} and \mathbf{b}_{iq} for the inequality constraints.

3.2 Objective Function Representation

First, the vector \mathbf{a}^T in the objective function is given by

$$\mathbf{a}^T = [a_1 \ \cdots \ a_I \ -c_1 \ \cdots \ -c_J \ 0 \ \cdots \ 0]_{1 \times (I+J+K-1)}$$

Next, the positive definite matrix \mathbf{G} in the objective function is given by

$$\mathbf{G} = \text{blockDiag} [\mathbf{U} \ \mathbf{W}_{\text{rr}}] = \begin{bmatrix} \mathbf{U} & \mathbf{0} \\ \mathbf{0} & \mathbf{W}_{\text{rr}} \end{bmatrix}_{(I+J+K-1) \times (I+J+K-1)} \quad (26)$$

where

$$\mathbf{U} = \text{diag} [2b_1 \ \cdots \ 2b_I \ 2d_1 \ \cdots \ 2d_J]_{(I+J) \times (I+J)} \quad (27)$$

$$\mathbf{W}_{\text{rr}} = 2\pi \begin{bmatrix} \sum_{k \neq 2} \mathbb{E}_{k2} & -\mathbb{E}_{23} & \cdots & -\mathbb{E}_{2K} \\ -\mathbb{E}_{32} & \sum_{k \neq 3} \mathbb{E}_{k3} & \cdots & -\mathbb{E}_{3K} \\ \vdots & \vdots & \ddots & \vdots \\ -\mathbb{E}_{K2} & -\mathbb{E}_{K3} & \cdots & \sum_{k \neq K} \mathbb{E}_{kK} \end{bmatrix}_{(K-1) \times (K-1)} \quad (28)$$

$$\mathbb{E} = \begin{bmatrix} 0 & \mathbb{I}(1 \leftrightarrow 2) & \mathbb{I}(1 \leftrightarrow 3) & \cdots & \mathbb{I}(1 \leftrightarrow K) \\ \mathbb{I}(2 \leftrightarrow 1) & 0 & \mathbb{I}(2 \leftrightarrow 3) & \cdots & \mathbb{I}(2 \leftrightarrow K) \\ \mathbb{I}(3 \leftrightarrow 1) & \mathbb{I}(3 \leftrightarrow 2) & 0 & \cdots & \mathbb{I}(3 \leftrightarrow K) \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ \mathbb{I}(K \leftrightarrow 1) & \mathbb{I}(K \leftrightarrow 2) & \mathbb{I}(K \leftrightarrow 3) & \cdots & 0 \end{bmatrix}_{K \times K} \quad (29)$$

$$\mathbb{I}(k \leftrightarrow m) = \begin{cases} 1 & \text{if either } km \text{ or } mk \in BR \\ 0 & \text{otherwise} \end{cases}$$

3.3 Equality Constraints Representation

Then, the equality constraint matrix \mathbf{C}_{eq}^T takes the form:

$$\mathbf{C}_{\text{eq}}^T = [\mathbf{II} \ -\mathbf{JJ} \ -\mathbf{B}'_{\text{r}}{}^T]_{K \times (I+J+K-1)}$$

where

$$\mathbf{II} = \begin{bmatrix} \mathbb{I}(1 \in I_1) & \mathbb{I}(2 \in I_1) & \cdots & \mathbb{I}(I \in I_1) \\ \mathbb{I}(1 \in I_2) & \mathbb{I}(2 \in I_2) & \cdots & \mathbb{I}(I \in I_2) \\ \vdots & \vdots & \ddots & \vdots \\ \mathbb{I}(1 \in I_K) & \mathbb{I}(2 \in I_K) & \cdots & \mathbb{I}(I \in I_K) \end{bmatrix}_{K \times I} \quad (30)$$

$$\mathbb{I}(i \in I_k) = \begin{cases} 1 & \text{if } i \in I_k \\ 0 & \text{if } i \notin I_k \end{cases}$$

$$\mathbf{J}\mathbf{J} = \begin{bmatrix} \mathbb{I}(1 \in J_1) & \mathbb{I}(2 \in J_1) & \cdots & \mathbb{I}(J \in J_1) \\ \mathbb{I}(1 \in J_2) & \mathbb{I}(2 \in J_2) & \cdots & \mathbb{I}(J \in J_2) \\ \vdots & \vdots & \ddots & \vdots \\ \mathbb{I}(1 \in J_K) & \mathbb{I}(2 \in J_K) & \cdots & \mathbb{I}(J \in J_K) \end{bmatrix}_{K \times J} \quad (31)$$

$$\mathbb{I}(j \in J_k) = \begin{cases} 1 & \text{if } j \in J_k \\ 0 & \text{if } j \notin J_k \end{cases}$$

$$\mathbf{B}'_{\mathbf{r}} = \begin{bmatrix} -B_{21} & \sum_{k \neq 2} B_{k2} & -B_{23} & \cdots & -B_{2K} \\ -B_{31} & -B_{32} & \sum_{k \neq 3} B_{k3} & \cdots & -B_{3K} \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ -B_{K1} & -B_{K2} & -B_{K3} & \cdots & \sum_{k \neq K} B_{kK} \end{bmatrix}_{(K-1) \times K} \quad (32)$$

$$B_{km} = \begin{cases} \frac{1}{x_{km}} > 0 & \text{if } km \text{ or } mk \in BR \\ 0 & \text{otherwise} \end{cases}$$

The associated equality constraint vector $\mathbf{b}_{\mathbf{eq}}$ takes the form:

$$\mathbf{b}_{\mathbf{eq}} = \left[\sum_{j \in J_1} p_{Lj}^F \quad \sum_{j \in J_2} p_{Lj}^F \quad \cdots \quad \sum_{j \in J_K} p_{Lj}^F \right]_{K \times 1}^{\mathbf{T}}$$

3.4 Inequality Constraints Representation

Finally, the inequality constraint matrix $\mathbf{C}_{\mathbf{iq}}$ takes the form as follows.

$$\mathbf{C}_{\mathbf{iq}}^{\mathbf{T}} = \left[\frac{\mathbf{MatrixT}}{\mathbf{MatrixG}} \right] = \left[\begin{array}{ccc} \mathbf{O}_{\mathbf{NI}} & \mathbf{O}_{\mathbf{NJ}} & \mathbf{Z}\mathbf{A}_{\mathbf{r}} \\ \mathbf{O}_{\mathbf{NI}} & \mathbf{O}_{\mathbf{NJ}} & -\mathbf{Z}\mathbf{A}_{\mathbf{r}} \\ \hline \mathbf{I}_{\mathbf{II}} & \mathbf{O}_{\mathbf{IJ}} & \mathbf{O}_{\mathbf{IK}} \\ -\mathbf{I}_{\mathbf{II}} & \mathbf{O}_{\mathbf{IJ}} & \mathbf{O}_{\mathbf{IK}} \\ \hline \mathbf{O}_{\mathbf{JI}} & \mathbf{I}_{\mathbf{JJ}} & \mathbf{O}_{\mathbf{JK}} \\ \mathbf{O}_{\mathbf{JI}} & -\mathbf{I}_{\mathbf{JJ}} & \mathbf{O}_{\mathbf{JK}} \end{array} \right]_{(2N+2I+2J) \times (I+J+K-1)}$$

where $\mathbf{O}_{\mathbf{NI}}$ is an $N \times I$ zero matrix, $\mathbf{O}_{\mathbf{NJ}}$ is an $N \times J$ zero matrix, $\mathbf{O}_{\mathbf{IJ}}$ is an $I \times J$ zero matrix, $\mathbf{O}_{\mathbf{IK}}$ is an $I \times (K-1)$ zero matrix, $\mathbf{O}_{\mathbf{JI}}$ is a $J \times I$ zero matrix, and $\mathbf{O}_{\mathbf{JK}}$ is a $J \times (K-1)$ zero matrix; $\mathbf{I}_{\mathbf{II}}$ is an $I \times I$ identity matrix and $\mathbf{I}_{\mathbf{JJ}}$ is a $J \times J$ identity matrix; and matrices \mathbf{Z} and $\mathbf{A}_{\mathbf{r}}$ are defined as follows.

Let \mathbf{BI} denote the listing of the N physically distinct branches $km \in BR$ constituting the transmission grid, lexicographically sorted as in a dictionary from lower to higher numbered nodes. Let \mathbf{BI}_n denote the n th branch listed in \mathbf{BI} . Then the *adjacency matrix* \mathbf{A} with entries of 1 for the “from” node and -1 for the “to” node can be expressed as follows:

$$\mathbf{A} = \begin{bmatrix} \mathbb{J}(1, \mathbf{BI}_1) & \mathbb{J}(2, \mathbf{BI}_1) & \cdots & \mathbb{J}(K, \mathbf{BI}_1) \\ \mathbb{J}(1, \mathbf{BI}_2) & \mathbb{J}(2, \mathbf{BI}_2) & \cdots & \mathbb{J}(K, \mathbf{BI}_2) \\ \vdots & \vdots & \ddots & \vdots \\ \mathbb{J}(1, \mathbf{BI}_N) & \mathbb{J}(2, \mathbf{BI}_N) & \cdots & \mathbb{J}(K, \mathbf{BI}_N) \end{bmatrix}_{N \times K} \quad (33)$$

where $\mathbb{J}(\cdot)$ is an indicator function defined as:

$$\mathbb{J}(k, \mathbf{BI}_n) = \begin{cases} +1 & \text{if } \mathbf{BI}_n \text{ takes the form } km \in BR \text{ for some node } m > k \\ -1 & \text{if } \mathbf{BI}_n \text{ takes the form } mk \in BR \text{ for some node } m < k \\ 0 & \text{otherwise} \end{cases}$$

for all nodes $k = 1, \dots, K$ and for all branches $n = 1, \dots, N$

Let the *reduced adjacency matrix* \mathbb{A}_r be defined as \mathbb{A} with its first column deleted. Thus, \mathbb{A}_r is expressed as

$$\mathbb{A}_r = \begin{bmatrix} \mathbb{J}(2, \mathbf{BI}_1) & \cdots & \mathbb{J}(K, \mathbf{BI}_1) \\ \mathbb{J}(2, \mathbf{BI}_2) & \cdots & \mathbb{J}(K, \mathbf{BI}_2) \\ \vdots & \ddots & \vdots \\ \mathbb{J}(2, \mathbf{BI}_N) & \cdots & \mathbb{J}(K, \mathbf{BI}_N) \end{bmatrix}_{N \times (K-1)} \quad (34)$$

The matrix \mathbf{Z} is defined as the diagonal matrix whose diagonal entries give the B_{km} values for all distinct connected branches $km \in BR$ ordered as in BI . That is,

$$\mathbf{Z} = \text{diag} [Z_1 \quad Z_2 \quad \cdots \quad Z_N]_{N \times N} \quad (35)$$

where $Z_n = B_{km}$ if BI_n (the n th element of BI) corresponds to branch $km \in BR$.

Let $P_{BI_n}^U = P_{km}^U$ if BI_n corresponds to branch $km \in BR$. The associated inequality constraint vector \mathbf{b}_{iq} can then be expressed as follows:

$$\mathbf{b}_{iq} = [-\mathbf{P}^U \quad -\mathbf{P}^U \quad \mathbf{Cap}^L \quad -\mathbf{Cap}^U \quad \mathbf{SLoad}^L \quad -\mathbf{SLoad}^U]_{(2N+2I+2J) \times 1}^T$$

where

$$\mathbf{P}^U = [P_{\mathbf{BI}_1}^U \quad P_{\mathbf{BI}_2}^U \quad \cdots \quad P_{\mathbf{BI}_N}^U]_{N \times 1}^T$$

$$\mathbf{Cap}^L = [Cap_1^L \quad Cap_2^L \quad \cdots \quad Cap_I^L]_{I \times 1}^T$$

$$\mathbf{Cap}^U = [Cap_1^U \quad Cap_2^U \quad \cdots \quad Cap_I^U]_{I \times 1}^T$$

$$\mathbf{SLoad}^L = [SLoad_1^L \quad SLoad_2^L \quad \cdots \quad SLoad_J^L]_{J \times 1}^T$$

$$\mathbf{SLoad}^U = [SLoad_1^U \quad SLoad_2^U \quad \cdots \quad SLoad_J^U]_{J \times 1}^T$$

4 Illustrative 5-Node Example

Now consider a five-node case for which the transmission grid is not completely connected; see Figure 1. Let five Generators and three LSEs be distributed across the grid as follows: Generators 1 and 2 are located at node 1; LSE 1 is located at node 2; Generator 3 and LSE 2 are located at node 3; Generator 4 and LSE 3 are located at node 4; and Generator 5 is located node 5.

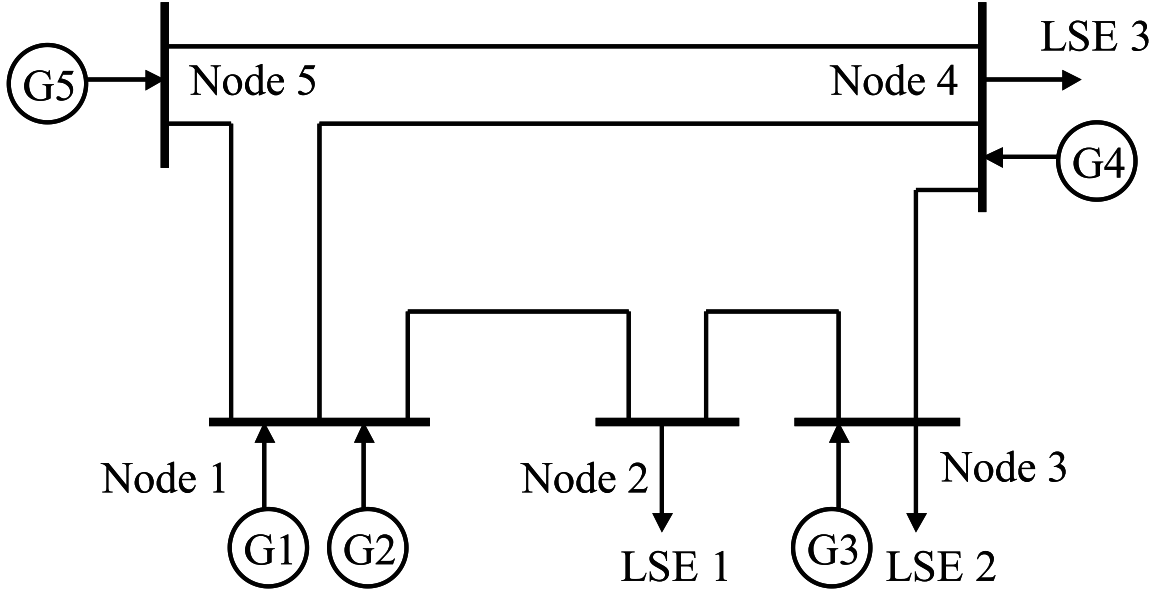


Figure 1: 5-Node Transmission Grid

4.1 5-Node Structural Form

This information implies the following structural configuration for the transmission grid:

$$I = 5; J = 3; K = 5; N = 6$$

$$I_1 = \{G1, G2\}, I_2 = \{\emptyset\}, I_3 = \{G3\}, I_4 = \{G4\}, I_5 = \{G5\};$$

$$J_1 = \{\emptyset\}, J_2 = \{LSE1\}, J_3 = \{LSE2\}, J_4 = \{LSE3\}, J_5 = \{\emptyset\};$$

$$BR = \{(1, 2), (1, 4), (1, 5), (2, 3), (3, 4), (4, 5)\}$$

The structural DC-OPF problem then takes the following form:

Minimize

$$\sum_{i=1}^5 [a_i \cdot p_{Gi} + b_i \cdot p_{Gi}^2] - \sum_{j=1}^3 [c_j \cdot p_{Lj}^S - d_j \cdot p_{Lj}^S{}^2] + \pi \left[[\delta_1 - \delta_2]^2 + [\delta_1 - \delta_4]^2 + [\delta_1 - \delta_5]^2 + [\delta_2 - \delta_3]^2 + [\delta_3 - \delta_4]^2 + [\delta_4 - \delta_5]^2 \right] \quad (36)$$

with respect to real power generation levels, real power price-sensitive loads, and voltage angles

$$p_{Gi}, i = 1, \dots, 5; p_{Lj}^S, j = 1, \dots, 3; \delta_k, k = 1, \dots, 5$$

subject to:

Real power balance constraint for each node $k = 1, \dots, 5$:

$$\sum_{i \in I_k} p_{Gi} - \sum_{j \in J_k} p_{Lj}^S - \sum_{km \text{ or } mk \in BR} P_{km} = \sum_{j \in J_k} p_{Lj}^F \quad (37)$$

where

$$P_{km} = B_{km} [\delta_k - \delta_m] \quad (38)$$

Real power thermal constraint for each branch $km \in BR$:

$$|P_{km}| \leq P_{km}^U \quad (39)$$

Real power operating capacity constraints for each Generator $i = 1, \dots, 5$:

$$Cap_i^L \leq p_{Gi} \leq Cap_i^U \quad (40)$$

Real power price-sensitive load constraints for each LSE $j = 1, \dots, 3$:

$$SLoad_j^L \leq p_{Lj}^S \leq SLoad_j^U \quad (41)$$

Voltage angle setting at reference node 1:

$$\delta_1 = 0 \quad (42)$$

4.2 5-Node Objective Function Representation

First, the solution vector \mathbf{x} takes the form

$$\mathbf{x} = [p_{G1} \ p_{G2} \ p_{G3} \ p_{G4} \ p_{G5} \ p_{L1}^S \ p_{L2}^S \ p_{L3}^S \ \delta_2 \ \delta_3 \ \delta_4 \ \delta_5]_{12 \times 1}^T$$

The vector \mathbf{a}^T in the objective function is given by

$$\mathbf{a}^T = [a_1 \ a_2 \ a_3 \ a_4 \ a_5 \ -c_1 \ -c_2 \ -c_3 \ 0 \ 0 \ 0 \ 0]_{1 \times 12}$$

Next, the positive definite matrix \mathbf{G} in the objective function is given by

$$\mathbf{G} = \text{blockDiag} [\mathbf{U} \ \mathbf{W}_{rr}] = \begin{bmatrix} \mathbf{U} & \mathbf{0} \\ \mathbf{0} & \mathbf{W}_{rr} \end{bmatrix}_{12 \times 12} \quad (43)$$

where

$$\mathbf{U} = \text{diag} [2b_1 \ 2b_2 \ 2b_3 \ 2b_4 \ 2b_5 \ 2d_1 \ 2d_2 \ 2d_3]_{8 \times 8} \quad (44)$$

$$\mathbf{W}_{\mathbf{r}\mathbf{r}} = 2\pi \begin{bmatrix} 2 & -1 & 0 & 0 \\ 1 & 2 & -1 & 0 \\ 0 & -1 & 3 & -1 \\ 0 & 0 & -1 & 2 \end{bmatrix}_{4 \times 4} \quad (45)$$

4.3 5-Node Equality Constraints Representation

Then, the equality constraint matrix $\mathbf{C}_{\mathbf{e}\mathbf{q}}^{\mathbf{T}}$ takes the form:

$$\mathbf{C}_{\mathbf{e}\mathbf{q}}^{\mathbf{T}} = [\mathbf{II} \quad -\mathbf{JJ} \quad -\mathbf{B}'_{\mathbf{r}}{}^{\mathbf{T}}]_{5 \times (12)}$$

where

$$\mathbf{II} = \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 1 \end{bmatrix}_{5 \times 5} \quad (46)$$

$$\mathbf{JJ} = \begin{bmatrix} 0 & 0 & 0 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \\ 0 & 0 & 0 \end{bmatrix}_{5 \times 3} \quad (47)$$

$$\mathbf{B}'_{\mathbf{r}} = \begin{bmatrix} -B_{21} & B_{21} + B_{23} & -B_{23} & 0 & 0 \\ 0 & -B_{32} & B_{32} + B_{34} & -B_{34} & 0 \\ -B_{41} & 0 & -B_{43} & B_{41} + B_{43} + B_{45} & -B_{45} \\ -B_{51} & 0 & 0 & -B_{54} & B_{51} + B_{54} \end{bmatrix}_{4 \times 5} \quad (48)$$

The associated equality constraint vector $\mathbf{b}_{\mathbf{e}\mathbf{q}}$ takes the form:

$$\mathbf{b}_{\mathbf{e}\mathbf{q}} = [0 \quad p_{L1}^F \quad p_{L2}^F \quad p_{L3}^F \quad 0]_{5 \times 1}^{\mathbf{T}}$$

4.4 5-Node Inequality Constraints Representation

Finally, the inequality constraint matrix $\mathbf{C}_{\mathbf{i}\mathbf{q}}$ takes the form as follows.

$$\mathbf{C}_{\mathbf{i}\mathbf{q}}^{\mathbf{T}} = \begin{bmatrix} \text{MatrixT} \\ \text{MatrixG} \\ \text{MatrixL} \end{bmatrix} = \begin{bmatrix} \mathbf{O}_{\mathbf{NI}} & \mathbf{O}_{\mathbf{NJ}} & \mathbf{Z}\mathbf{A}_{\mathbf{r}} \\ \mathbf{O}_{\mathbf{NI}} & \mathbf{O}_{\mathbf{NJ}} & -\mathbf{Z}\mathbf{A}_{\mathbf{r}} \\ \hline \mathbf{II} & \mathbf{O}_{\mathbf{IJ}} & \mathbf{O}_{\mathbf{IK}} \\ -\mathbf{II} & \mathbf{O}_{\mathbf{IJ}} & \mathbf{O}_{\mathbf{IK}} \\ \hline \mathbf{O}_{\mathbf{JI}} & \mathbf{I}_{\mathbf{JJ}} & \mathbf{O}_{\mathbf{JK}} \\ \mathbf{O}_{\mathbf{JI}} & -\mathbf{I}_{\mathbf{JJ}} & \mathbf{O}_{\mathbf{JK}} \end{bmatrix}_{28 \times 12}$$

where

$$\mathbf{BI} = [(1, 2), (1, 4), (1, 5), (2, 3), (3, 4), (4, 5)]_{6 \times 1}^T \quad (49)$$

$$\mathbf{Z} = \text{diag} [B_{12} \ B_{14} \ B_{15} \ B_{23} \ B_{34} \ B_{45}]_{6 \times 6} \quad (50)$$

$$\mathbb{A}_{\mathbf{r}} = \begin{bmatrix} -1 & 0 & 0 & 0 \\ 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & -1 \\ 1 & -1 & 0 & 0 \\ 0 & 1 & -1 & 0 \\ 0 & 0 & 1 & -1 \end{bmatrix}_{6 \times 4} \quad (51)$$

Hence the complete matrix $\mathbf{C}_{\text{iq}}^{\text{T}}$ can be found as

$$\mathbf{C}_{\text{iq}}^{\text{T}} = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -B_{12} & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -B_{14} & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -B_{15} \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & B_{23} & -B_{23} & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & B_{34} & -B_{34} & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & B_{45} & -B_{45} \\ \hline 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & B_{12} & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & B_{14} & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & B_{15} \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -B_{23} & B_{23} & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -B_{34} & B_{34} & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -B_{45} & B_{45} \\ \hline 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ \hline -1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & -1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & -1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & -1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ \hline 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ \hline 0 & 0 & 0 & 0 & 0 & 0 & -1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & -1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -1 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}_{28 \times 12}$$

The associated inequality constraint vector \mathbf{b}_{iq} can be expressed as follows:

$$\mathbf{b}_{\text{iq}} = \left[-\mathbf{P}^{\text{U}} \quad -\mathbf{P}^{\text{U}} \quad \mathbf{Cap}^{\text{L}} \quad -\mathbf{Cap}^{\text{U}} \quad \mathbf{SLoad}^{\text{L}} \quad -\mathbf{SLoad}^{\text{U}} \right]_{28 \times 1}^{\text{T}}$$

where

$$\mathbf{P}^{\text{U}} = \left[P_{12}^{\text{U}} \quad P_{14}^{\text{U}} \quad P_{15}^{\text{U}} \quad P_{23}^{\text{U}} \quad P_{34}^{\text{U}} \quad P_{45}^{\text{U}} \right]_{6 \times 1}^{\text{T}}$$

$$\mathbf{Cap}^{\text{L}} = \left[Cap_1^{\text{L}} \quad Cap_2^{\text{L}} \quad Cap_3^{\text{L}} \quad Cap_4^{\text{L}} \quad Cap_5^{\text{L}} \right]_{5 \times 1}^{\text{T}}$$

$$\mathbf{Cap}^{\text{U}} = \left[Cap_1^{\text{U}} \quad Cap_2^{\text{U}} \quad Cap_3^{\text{U}} \quad Cap_4^{\text{U}} \quad Cap_5^{\text{U}} \right]_{5 \times 1}^{\text{T}}$$

$$\mathbf{SLoad}^{\text{L}} = \left[SLoad_1^{\text{L}} \quad SLoad_2^{\text{L}} \quad SLoad_3^{\text{L}} \right]_{3 \times 1}^{\text{T}}$$

$$\mathbf{SLoad}^{\text{U}} = \left[SLoad_1^{\text{U}} \quad SLoad_2^{\text{U}} \quad SLoad_3^{\text{U}} \right]_{3 \times 1}^{\text{T}}$$

Table 1: DC OPF Admissible Exogenous Variables

Variable	Description	Admissibility Restrictions
K	Total number of transmission grid nodes	$K > 0$
N	Total number of physically distinct network branches	$N > 0$
I	Total number of Generators	$I > 0$
J	Total number of LSEs	$J > 0$
I_k	Set of Generators located at node k	$\text{Card}(\cup_{k=1}^K I_k) = I$
J_k	Set of LSEs located at node k	$\text{Card}(\cup_{k=1}^K J_k) = J$
S_o	Base apparent power (in three-phase MVAs)	$S_o \geq 1$
V_o	Base voltage (in line-to-line kVs)	$V_o > 0$
V_k	Voltage magnitude (in kVs) at node k	$V_k = V_o, k = 1, \dots, K$
km	Branch connecting nodes k and m (if one exists)	$k \neq m$
BR	Set of all physically distinct branches $km, k < m$	$BR \neq \emptyset$
x_{km}	Reactance (ohms) for branch km	$x_{km} = x_{mk} > 0, km \in BR$
B_{km}	$[1/x_{km}]$ for branch km	$B_{km} = B_{mk} > 0, km \in BR$
P_{km}^U	Thermal limit (MWs) for real power flow on km	$P_{km}^U > 0, km \in BR$
δ_1	Reference node 1 voltage angle (in radians)	$\delta_1 = 0$
a_i, b_i	Cost coefficients for Generator i	$b_i > 0, i = 1, \dots, I$
Cap_i^L	Lower real power operating capacity for Generator i	$Cap_i^L \geq 0, i = 1, \dots, I$
Cap_i^U	Upper real power operating capacity for Generator i	$Cap_i^U > 0, i = 1, \dots, I$
$FCost_i$	Fixed costs (hourly prorated) for Generator i	$FCost_i \geq 0, i = 1, \dots, I$
c_j, d_j	Demand coefficients for LSE j	$c_j, d_j > 0, j = 1, \dots, J$
$SLoad_j^L$	Lower real power price-sensitive load limit for LSE j	$SLoad_j^L \geq 0, j = 1, \dots, J$
$SLoad_j^U$	Upper real power price-sensitive load limit for LSE j	$SLoad_j^U \leq c_j/[2d_j], j = 1, \dots, J$
p_{Lj}^F	Price-insensitive fixed real power load for LSE j	$p_{Lj}^F \geq 0, j = 1, \dots, J$

Table 2: DC OPF Endogenous Variables

Variable	Description
p_{Gi}	Real power generation (MWs) supplied by Generator $i = 1, \dots, I$
p_{Lj}^S	Price-sensitive real power load (MWs) demanded by LSE $j = 1, \dots, J$
δ_k	Voltage angle (in radians) at node $k = 2, \dots, K$
P_{km}	Real power (MWs) flowing in branch $km \in BR$