

Optimal Sensor Placement within a Hybrid Dense Sensor Network using an Adaptive Genetic Algorithm with Learning Gene Pool

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Abstract

This work develops optimal sensor placement within a hybrid dense sensor network used in the construction of accurate strain maps for large-scale structural components. Realization of accurate strain maps is imperative for improved strain-based fault diagnosis and prognosis health management in large-scale structures. Here, an objective function specifically formulated to reduce type I and II errors and an adaptive mutation-based genetic algorithm for the placement of sensors within the hybrid dense sensor network are introduced. The objective function is based on the linear combination method and validates sensor placement while increasing information entropy. Optimal sensor placement is achieved through a genetic algorithm that leverages the concept that not all potential sensor locations contain the same level of information. The level of information in a potential sensor location is taught to subsequent generations through updating the algorithm's gene pool. The objective function and genetic algorithm are experimentally validated for a cantilever plate under three loadings cases. Results demonstrate the ability of the learning gene pool to effectively and repeatedly find a Pareto-optimal solution faster than its non-adaptive gene pool counterpart.

Keywords

Optimal sensor placement, Structural health monitoring, Dense sensor network, Sensor Network, Genetic Algorithm, Strain Maps, Sensing Skin, Large Area Electronics

Introduction

Structural health monitoring (SHM) is the automation of the damage detection, localization, and prognosis tasks. From SHM follows Prognostics and health management (PHM), which focuses on predicting the remaining useful life of the system based on the inferred health and making optimal (often profit-maximizing) decisions on operations and maintenance (O&M)^{1,2}. Of particular interest to the authors is SHM/PHM of wind turbine blades, where the benefits of condition based maintenance are well understood^{2–4}. For examples, the use of PHM combined with a well-designed SHM system can enable smart load management for damaged wind turbine blades resulting in reduced operating cost and increased blade life⁵.

The success of an SHM/PHM system depends heavily on the availability of sensor data and the ability to detect, localize, and quantify a change in health state within the data set. This task becomes increasingly challenging for larger scale systems because of the lack of scalability of existing sensing solutions⁶. A solution is to deploy sensor networks, which have been promoted by significant technological advances in sensing, wireless communication, and data processing techniques⁷. Also, recent advances in polymers have encouraged the development of flexible electronics, which can be used to form dense sensor networks (DSNs) to monitor large areas, at low cost. Such applications are

often compared to sensing skins, which often consist of discrete rigid or semi-rigid sensing nodes (cells) mounted on a flexible sheet (skin)^{8,9}.

The authors have previously developed a capacitance-based sensing skin, termed the soft elastomeric capacitor (SEC). The proposed SEC was designed to be inexpensive with an easily scalable manufacturing process¹⁰. A particular feature of the SEC is that it measures additive in-plane strain, instead of a traditional measurement of the linear strain along a single direction. When used in a DSN configuration, the SEC is able to monitor local additive strain over large areas. The signal can be used to reconstruct strain maps, provided that the additive strain is decomposed into linear strain components along two orthogonal directions. Downey *et. al* presented an algorithm⁶ designed to leverage a DSN

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42 configuration along with other off-the-shelf sensors (termed
43 hybrid DSN or HDSN) to enable strain field decomposition.
44 The algorithm assumed a shape function and classical
45 Kirchhoff plate theory, as well as boundary conditions, and
46 solved for the coefficients of the shape function using a
47 least squares estimator (LSE). Results demonstrated that
48 such algorithm had great promise at providing strain map
49 measurements, but that its performance was dependent on
50 sensor placement, and that it was critical to develop an
51 optimal sensor placement (OSP) strategy for the placement
52 of sensors within an HDSN.

53 The objective of OSP is to identify the optimal locations
54 of sensors such that the measured data provide a rich
55 level of information. OSP can be expressed as a classical
56 combinatorial problem generalized as: given a set of n
57 candidate locations, find m locations, with $m < n$, providing
58 the best possible performance. For optimization problems
59 where m or n are limited, the solution can be solved
60 using a trial-and-error approach. However, for large sizes
61 of m or n , the search becomes computationally demanding;
62 a systematic and efficient sensor placement approach is
63 required. Naturally, two questions arise with regard to
64 sensor placement: which type of sensor placement objective
65 function should be implemented and what algorithm can be
66 applied for OSP¹¹.

67 A large number of formulations of the objective function
68 have been developed in prior literature. These can be grouped
69 as: 1) Fisher information matrix (FIM)^{12–14} for minimizing
70 the covariance of the parameter estimation error; 2) modal
71 assurance criterion (MAC)¹⁵ for minimizing the maximum
72 off-diagonal value (or the highest degree of linearity between
73 different modal vectors) in the MAC matrix; 3) information
74 entropy¹⁶ for minimizing the uncertainty in model parameter
75 estimates; 4) probability of detection¹⁷ for maximizing
76 probability of damage detection or minimizing false alarm
77 rate; and 5) mean squared error in estimating structural
78 parameter of interest (e.g., mode shape¹⁴). An objective
79 function chosen to validate sensor placement will vary
80 greatly with respect to the application. Certain objective
81 functions may perform well in selecting sensor locations for
82 global parameter identification (e.g., changes in stiffness)
83 but fail to detect changes in local damage cases (e.g.,
84 crack growth). A solution is the formulation of sensor
85 placement as a multi-objective optimization problem¹⁸. For
86 the case of optimizing several conflicting objectives, there
87 does not exist a single solution that simultaneously optimizes
88 every considered objective. However, there is a set of
89 (possibly infinite) optimal solutions known as Pareto-optimal
90 solutions. These solutions reside on the Pareto frontier.

91 After an appropriate formulation of the objective function
92 is determined, the remaining task is to select the optimal
93 sensor locations from the predefined set of candidate
94 locations. Various solvers for this discrete optimization
95 problem have been proposed. In SHM, sensor placement
96 for the extraction of modal shapes has been extensively
97 researched due to the significant importance of modal
98 shapes in structural model updating^{7;11;13;19;20}. Some solvers
99 that show good promise for optimizing sensor placement
100 within an HDSN are reviewed here. Sequential sensor
101 placement offers a systematic approach by selecting the
102 sensor location that results in the highest addition in

103 information entropy and setting that as the first optimal
104 sensor position. All subsequent sensor location selections are
105 made in a similar manner. While computationally efficient,
106 sequential sensor placement solvers lack the ability to find
107 optimal sensor locations because its search tree is limited
108 by previously selected sensor locations^{12;16}. The monkey
109 search algorithm, in its most basic form, seeks to expand
110 on the sequential sensor placement in searching multiple
111 branches of the search tree for local optimal solutions. The
112 algorithm is capable of looking at and jumping to others
113 branches whose objective values exceed those of the current
114 solutions allowing it to search multiple branches rapidly¹⁵.
115 Particle swarm optimization addresses the problem of sensor
116 placement by allowing set of particles to transverse a search-
117 space while each particle interacts with the global best-
118 fit particle. In comparison to the solvers presented above,
119 swarm optimization does not build an OSP solution but
120 rather seeks to improve on a candidate solution (often termed
121 an initial guess) until a solution of acceptable performance is
122 found¹⁴.

123 Genetic algorithms (GAs), based on the mutation of genes
124 over generations, have been proposed as an effective solution
125 to the limited search space of the sequential sensor placement
126 and monkey search algorithms¹³. They are bio-inspired
127 global probabilistic search algorithms that mimic nature's
128 ability to pass genes from one generation to the next²¹. GAs
129 greatly lend themselves for use as an OSP solver. Sensor
130 locations can be directly linked to genes that are mutated
131 through the generations and have been widely used for the
132 simultaneous placement of sensors in OSP²². After multiple
133 generations, only the strongest genes remain and form the set
134 of sensor locations for optimal sensor placement²⁰.

135 In this paper, a specialized case of OSP is presented for
136 application to an HDSN. The HDSN consists of a sensing
137 skin capable of covering large areas at low cost for SHM
138 of large-scale components. The intention is to equip the
139 HDSN with optimally placed resistive strain gauges (RSGs)
140 for the realization of accurate strain maps through providing
141 precise strain measurements at key locations. It will enable
142 HDSNs for strain-based fault diagnosis and prognosis health
143 management techniques and empower low-cost large-area
144 electronics such as the SEC. Sensor placement design for an
145 HDSN should attain three objectives: 1) optimize the sharing
146 of sensor network resources; 2) reduce type I errors (false
147 positive for damage detection damage); and 3) reduce type
148 II errors (fail to detect damage). All three objectives are
149 considered in the OSP developed for increasing the accuracy
150 of the reconstructed strain maps. Sharing of sensor network
151 resources allows the HDSN to increase information entropy
152 without the cost and complexity of additional sensors. A
153 sensor placement algorithm that reduces the probability of
154 type I errors can reduce maintenance cost and provide the
155 operator with a high level of confidence in the system²³.
156 Additionally, the choice of sensor placement that reduces
157 the probability of type II errors may reduce the risk of
158 catastrophic failure and the potential for loss-of-life events.
159 Sharing of sensor resources within the HDSN is obtained
160 through the implementation of the enhanced LSE algorithm,
161 while the reduction of type I and type II errors is obtained
162 through the consideration of multiple objectives.

This work introduces an objective function based on the linear combination method and validates simultaneous sensor placement while increasing information entropy. The objective function allows for a sensor placement that decreases the likelihood of the SHM system experiencing a type I or type II error. The single objective function and adaptive GA with learning gene pool are experimentally validated through an OSP problem formulated for a cantilever plate under three loadings cases.

For a OSP solver, we adopt a mutation-based GA through investigating the concept that not all sensor locations in m offer the same information potential. We introduce an adaptive mutation-based GA with a gene pool that is capable of learning as the generations advance. Utilizing the basic knowledge that some sensor locations inherently add more information to the system than others, the adaptive GA continuously alters the algorithm's gene pool in reference to the individual gene's effect on offspring fitness.

Contributions in this article are threefold: 1) definition of a multi-objective optimization problem to reduce the occurrence of type I and type II errors in an SHM system, and solving the multi-objective problem as a single objective problem by linear scalarization; 2) development of the case study of an adaptive mutation-based GA with learning gene pool for placement of sensors within an HDSN; 3) formulation of the optimal deployment of an HDSN utilizing flexible electronics to monitor local changes on a global scale and RGSSs for the enforcement of boundary conditions.

Background

This section provides the background on the SEC sensor, including its electro-mechanical model and reviews the enhanced LSE algorithm developed in previous work.

Soft Elastomeric Capacitor

The SEC is a robust and highly elastic flexible electronic that transduces a change in its geometry (i.e., strain) into a measurable change in capacitance. The fabrication process of the SEC was documented by Laflamme *et. al*²⁴. The sensor's dielectric is composed of a styrene-ethylene-butylene-styrene (SEBS) block co-polymer matrix filled with titania to increase both its durability and permittivity. Its conductive plates are also fabricated from an SEBS but filled with carbon black particles. All of the components used in the fabrication process are commercially available, and its fabrication process is relatively simple, making the technology highly scalable.

The SEC is designed to measure in-plane strain ($x - y$ plane in Figure 1) and is pre-stretched and adhered to the monitored substrate using a commercial two-part epoxy. Assuming a relatively low sampling rate ($< 1 \text{ kHz}$), the SEC can be modeled as a non-lossy capacitor with capacitance C , given by the parallel plate capacitor equation,

$$C = e_0 e_r \frac{A}{h} \quad (1)$$

where $e_0 = 8.854 \text{ pF/m}$ is the vacuum permittivity, e_r is the polymer relative permittivity, $A = d \cdot l$ is the sensor area of width d and length l , and h is the thickness of the dielectric as denoted in Figure 1.

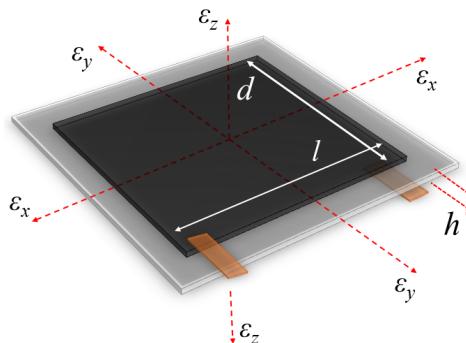


Figure 1. Sketch of a SEC's geometry with reference axes.

Assuming small strain, an expression relating the sensor's change in capacitance to signal can be expressed as

$$\frac{\Delta C}{C} = \lambda(\varepsilon_x + \varepsilon_y) \quad (2)$$

where $\lambda = 1/(1 - \nu)$ represents the gauge factor of the sensor, with ν being the sensor material's Poisson ratio. For SEBS, $\nu \approx 0.49$, which yields a gauge factor $\lambda \approx 2$. The electro-mechanical model is derived in reference²⁵. Equation (2) shows that the signal of the SEC varies as a function of the additive strain $\varepsilon_x + \varepsilon_y$. The linearity of the derived electro-mechanical model holds for mechanical responses up to 15 Hz²⁵. An altered electro-mechanical model has been derived in²⁶ for modeling mechanical responses up to 40 Hz but is not shown here for brevity. The SEC's electro-mechanical model has been validated at numerous occasions for both static and dynamic strain, see references^{24–26} for instance. Additionally, the SEC has been shown to operate successfully in the relatively noisy environment of a wind tunnel mounted inside a wind turbine blade model²⁷.

Strain Decomposition Algorithm

The SEC signal comprises the additive in-plane strain components, as expressed in Equation (2). The enhanced LSE algorithm was designed to decompose strain maps by leveraging an HDSN configuration. The algorithm is presented in⁶ and summarized in what follows.

The enhanced LSE algorithm assumes a parametric displacement shape function. For simplicity, consider a cantilever plate that extends into the $x-y$ plane with a constant thickness c , and fixed along one edge (at $x = 0$). A p^{th} order polynomial is selected due to its mathematical simplicity to approximate the plates deflection shape. The deflection shape w is expressed as

$$w(x, y) = \sum_{i=2, j=1}^p b_{ij} x^i y^j \quad (3)$$

where $b_{i,j}$ are regression coefficients, with $i > 1$ to satisfy the displacement boundary condition on the clamped edge where $w_{(0,y)} = 0$. Taking an HDSN with m sensors and collecting displacements at sensors' locations in a vector \mathbf{W} , Equation (3) becomes $\mathbf{W} = [w_1 \dots w_k \dots w_m]^T = \mathbf{H}\mathbf{B}$. Where \mathbf{H} encodes sensor location information and \mathbf{B} is the regression

coefficients matrix such that $\mathbf{B} = [b_1 \dots b_a]^T$ where b_a represents the last regression coefficient.

The \mathbf{H} location matrix is defined as $\mathbf{H} = [\Gamma_x \mathbf{H}_x | \Gamma_y \mathbf{H}_y]$ where \mathbf{H}_x and \mathbf{H}_y account for the SEC's additive strain measurements. Γ_x and Γ_y are added as appropriately defined diagonal weight matrices holding the scalar sensor weight values $\gamma_{x,k}$ and $\gamma_{y,k}$, associated with the k -th sensor. For instance, an RSG sensor k orientated in the x direction will take weight values $\gamma_{x,k} = 1$ and $\gamma_{y,k} = 0$. Virtual sensors, treated as RSG sensors with known signals, may also be added into \mathbf{H} . Virtual sensors are analogous to RSG sensors, except they are located at points where the boundary condition can be assumed to a high degree of certainty. The matrices are developed from quantities contained in Equation (3);

$$\mathbf{H}_x = \mathbf{H}_y = \begin{bmatrix} y_1^n & x_1 y_1^{n-1} & \dots & x_1^{n-1} y_1 & x_1^n \\ y_m^n & x_m y_m^{n-1} & \dots & x_m^{n-1} y_m & x_m^n \end{bmatrix} \quad (4)$$

Linear strain functions ε_x and ε_y along the x and y directions, respectively, can be obtained from Equation 3 through the enforcement of Kirchhoffs plate theory as;

$$\varepsilon_x(x, y) = -\frac{c}{2} \frac{\partial^2 w(x, y)}{\partial x^2} = \Gamma_x \mathbf{H}_x \mathbf{B}_x \quad (5)$$

$$\varepsilon_y(x, y) = -\frac{c}{2} \frac{\partial^2 w(x, y)}{\partial y^2} = \Gamma_y \mathbf{H}_y \mathbf{B}_y \quad (6)$$

where $\mathbf{B} = [\mathbf{B}_x | \mathbf{B}_y]^T$.

Linear strains at sensors' locations along the x and y directions can be obtained from sensors transducing $\varepsilon_x(x, y)$ and $\varepsilon_y(x, y)$. Signal vector \mathbf{S} is constructed in terms of the sensors strain signal $\mathbf{S} = [s_1 \dots s_k \dots s_m]^T$. Thereafter, the regression coefficient matrix \mathbf{B} can be estimated using an LSE:

$$\hat{\mathbf{B}} = (\mathbf{H}^T \mathbf{H})^{-1} \mathbf{H}^T \mathbf{S} \quad (7)$$

where the hat denotes an estimation. It results that the estimated strain maps can be reconstructed using

$$\hat{\mathbf{E}}_x = \Gamma_x \mathbf{H}_x \hat{\mathbf{B}}_x \quad \hat{\mathbf{E}}_y = \Gamma_y \mathbf{H}_y \hat{\mathbf{B}}_y \quad (8)$$

where \mathbf{E}_x and \mathbf{E}_y are vectors containing the estimated strain in the x and y directions for sensors transducing $\varepsilon_x(x, y)$ and $\varepsilon_y(x, y)$, respectively.

An HDSN without a sufficient number of RSGs will result in \mathbf{H} being multi-collinear because \mathbf{H}_x and \mathbf{H}_y share multiple rows, resulting in $\mathbf{H}^T \mathbf{H}$ being non-invertible. This can be avoided by integrating a sufficient number of RSGs into the HDSN.

Optimal sensor placement

This section proposes a single objective function that solves the multi-objective problem of decreasing the likelihood of type I and type II errors through the placement of RSGs in the HDSN. The objective function is based on the linear combination method, borrowed from the field of robust design²⁸ that seeks to find a solution on the Pareto frontier. Thereafter, an adaptive GA specially formulated through the use of a learning gene pool for applications in sensor placement is introduced.

Bi-optimization objective function

The occurrence of type I and type II errors in a structure depends, in part, on the strain-based fault diagnostic techniques applied to the extracted strain maps. In general, a type I error is the incorrect calcification of a healthy state as a damage state caused by consistently inaccurate strain maps being construed for a structural component. In comparison, a type II error is the failure to detect a structural fault that the properly selected strain-based fault diagnostic technique was designed to detect.

For the purpose of reducing the occurrence of type I errors within the HDSN's extracted strain maps, an optimization problem based on minimizing the mean absolute error (MAE) between the system and its estimated response is utilized. The use of MAE for validation provides a simple yet effective representation of how a structure will perform under static and dynamic loading. However, sensor placement validation based solely on the sensor network's MAE value may result in locations of high disagreement between the estimated and real systems. In the case of a monitored system, such an occurrence could result in a system component being stressed past its design limit, leading to an undetected localized failure (i.e. type II error). To reduce the occurrence of type II errors in an HDSN, a second optimization problem based on minimizing the maximum difference between the system and its estimated response per any individual point on a strain map is introduced, defined as β . The bi-objective optimization problem for placing m sensors can be formulated as,

$$\begin{aligned} & \underset{\mathbf{P}}{\text{minimize}} \quad f(\mathbf{P}) = (\text{MAE}(\mathbf{P}), \beta(\mathbf{P})) \\ & \text{subject to} \quad \mathbf{P} = [p_1 \dots p_m]^T \in \mathbb{P} \\ & \quad 0 \leq m \leq n \end{aligned} \quad (9)$$

where \mathbf{P} is a unique vector consisting of m unique sensor locations p taken from the global set of sensor locations, \mathbb{P} , with size n .

These multi-optimization problems can be combined to form a single objective optimization function with solutions that lie on the Pareto frontier. While various methods have been proposed for finding solutions on the Pareto frontier, a straightforward scalarization approach formulated as a linear combination method is applied here. The linear combination method finds the minimum of a weighted linear combination of objectives, resulting in a Pareto-optimal solution. This approach allows for trade-offs between the two objectives, thereby increasing the usability of the optimization function. The single objective problem for optimizing the placement of m sensors can be formulated as,

$$\begin{aligned} & \underset{\mathbf{P}}{\text{minimize}} \quad \text{fit} = (1 - \alpha) \frac{\text{MAE}(\mathbf{P})}{\text{MAE}'} + \alpha \frac{\beta(\mathbf{P})}{\beta'} \\ & \text{subject to} \quad \mathbf{P} = [p_1 \dots p_m]^T \in \mathbb{P} \\ & \quad 0 \leq m \leq n \\ & \quad 0 \leq \alpha \leq 1 \end{aligned} \quad (10)$$

where α is a user-defined scalarization factor to weight both objective functions. MAE' and β' are factors used for normalizing MAE and β . The optimization problem expressed in Equation (10) can be converted to a MAE value minimization problem for $\alpha = 0$, or a β minimization

problem for $\alpha = 1$. Selection of an appropriate value for α is based on the abilities of the selected strain-based fault detection techniques to avoid type I and type II errors. Additionally, selection of α depends on the structure's ability to tolerate type I or type II errors.

Adaptive genetic algorithm

The proposed adaptive GA leverages the intuitive idea that some sensor locations (p_k) add little or no information (i.e. low-information gene) to the estimated system when selected for use in a set (i.e. offspring) of potential sensors locations P . Conversely, some genes add a measurable amount of information to the system when selected for use in P (i.e. high-information gene). This concept is enforced into the GA through the use a learning gene pool. The proposed adaptive GA introduces a selection weight δ_k to each gene. Selection weights evolve with each generation through a percentage change ($\Delta\%$). Therefore, increasing the likelihood that a high-information gene is selected in the next generation from the gene pool:

$$\delta_{k,\text{generation}+1} = \delta_{k,\text{generation}} * \left(1 + \frac{\Delta\%}{100}\right) \quad (11)$$

Here k is a high-information gene from the current generation. Selection weights also reduce likelihood that a low-information gene is selected

$$\delta_{k,\text{generation}+1} = \delta_{k,\text{generation}} * \left(1 - \frac{\Delta\%}{100}\right) \quad (12)$$

where k is a low-information gene. Bounding the maximum and minimum δ values ensures that ensure that all genes are carried forward, and no genes dominate the gene pool.

Algorithm 1 Adaptive genetic algorithm using learning gene pool.

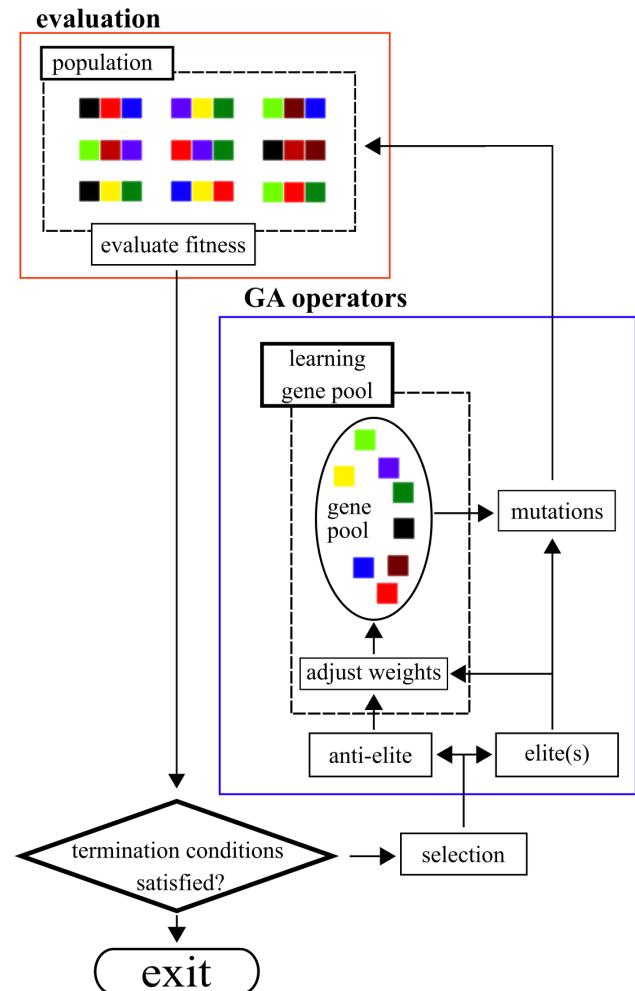
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1:  $P_{\text{elite}} = \text{initial guess}$ 
2: for generation count do
3:   mutate  $P_{\text{elite}}$  into  $P_{\text{population}}$ 
4:   for population count do
5:     generate LSE strain maps
6:     calculate fit
7:   end for
8:    $P_{1\text{-end}} = \text{ordered } P_{\text{population}} f(\text{fit})$ 
9:    $P_{\text{elite}} = P_1$ 
10:  adjust  $\delta_k$  correlating to  $p_{\text{elite}}$ 
11:   $P_{\text{anti-elite}} = P_{\text{end}}$ 
12:  adjust  $\delta_k$  correlating to  $p_{\text{anti-elite}}$ 
13: end for
```

The proposed GA framework is presented in Algorithm 1. Here, P_{elite} is the best performing P vector containing unique sensor locations that comprise the HDSN layout with the best fit. Conversely, $P_{\text{anti-elite}}$ is a vector containing the sensor locations that achieve the worst fit. Lastly, $P_{\text{population}}$ is the array of vectors that contains all sensor location vectors tested and can be arranged into $P_{1\text{-end}}$ based on the performance of these sensor location vectors. Figure 2 diagrams the GA flow.

While multiple variations for the adjustment of selection weights are possible, this work will focus on a simple

two-part updating technique. First, the elite offspring from a population is extracted, where all genes in P_{elite} are considered high-information genes. Next, the lowest performing offspring is extracted, where genes in $P_{\text{anti-elite}}$ are considered low-information genes. Thereafter, gene weights δ are adjusted by $\Delta\%$ as shown in Equations 11 and 12.



measuring ε_x or ε_y along the x and y axes as indicated in Figure 3. RSGs were arbitrarily located on the plate with the considerations that an equal number of RSGs measure ε_x and ε_y and that the RSGs are relatively evenly distributed.

Three different displacement-controlled load cases were selected and applied to the plate: load case I) an upward uniform displacement of 125 mm along the free edge; load case II) a downward uniform displacement of 97 mm along the free edge; and load case III) a twist of 43 degrees with reference to the initial plane. Each test consisted of three 15-second sets of unloaded, loaded, and unloaded conditions, for a total of 45 seconds.

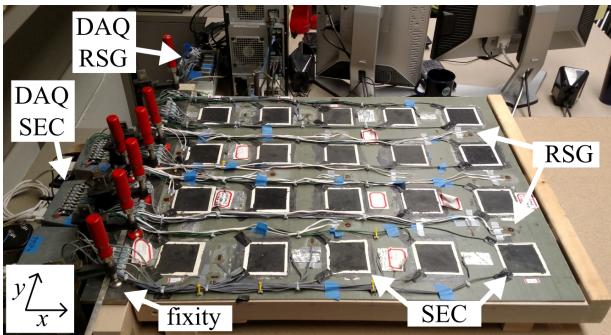


Figure 3. Experimental HDSN on fiberglass substrate.

Separate data acquisition (DAQ) hardware is used for the measurement of the SEC and RSG sensors, as annotated in Figure 3. RSG measurements are recorded at 100 Hz using a National Instruments cDAQ-9174 with four 24-bit 350 Ω quarter-bridge modules (NI-9236). SEC measurements are recorded at 25 Hz using a 16-bit capacitance-to-digital converter, PCAP-02, mounted inside the metal project boxes.

Signal Processing

A representative SEC signal is shown in Figure 4. Here, the capacitance signal is acquired from an SEC sensor under tension (top row, second from left, as shown Figure 3(b)) during load case II. Unfiltered data is presented in Figure 4(a). While the acquired sensor signal is relatively noisy, the noise is Gaussian as represented in the Q-Q plot in Figure 4(b). The oversampled signal is then decimated providing a single displaced measurement of greater resolution²⁹ for use in the Enhanced LSE algorithm. Given the static nature of the current work, this technique was found to provide acceptable results.

Algorithm configuration

Validation of the proposed adaptive GA with learning gene pool is performed for the case of $m = 10$ (RGS sensor locations), $n = 46$ (RSG candidate locations). An HDSN of 20 SECs and 10 RSGs was selected due to its ability to generate a viable estimation of the real system⁶, while still providing a sufficient search space. The estimated strain map is validated against the real strain map, as reconstructed using all 46 RSGs.

A single set of optimized sensor placement locations (\mathbf{P}) is obtained for the experimental HDSN. The final sensor configuration is the set of locations that best reproduce all six strain maps, three for ε_x and three for ε_y , under the three

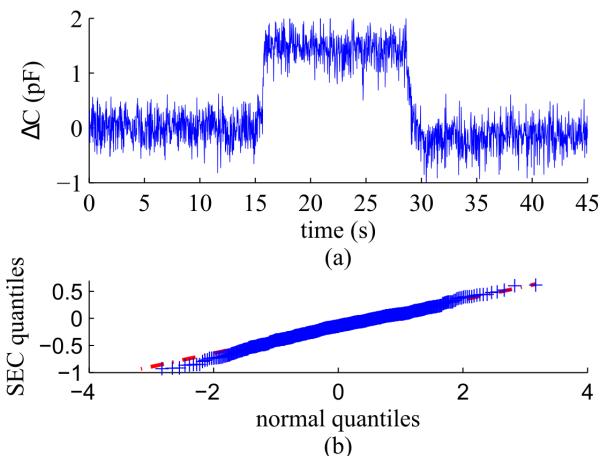


Figure 4. Representative SEC signal: (a) time series for test under load case II, (b) Q-Q plot for the SEC signal under load.

loading cases. Estimated strain maps are produced using the enhanced LSE algorithm presented in the background section. Additionally, five virtual sensor nodes are added along the fixity such that $\varepsilon_y = 0$. The sensors nodes are evenly spaced, placed at $x = 0$, $y = 0.10, 0.21, 0.31, 0.42$ and 0.52 m. Virtual sensors are not placed at the corners to account for edge effects present in the plate.

A set of initial sensor locations are needed to develop the normalization factors, MAE' and β' , used in Equation 9. To provide \mathbf{P} , a guess a set of 50 randomly selected sensor placement locations were produced. Using a single objective optimization function minimizing the MAE a best-of-50 sensor placement was obtained. The optimization function minimizing only the MAE was chosen over that minimizing β , since the former maximizes the fit over all six strain maps and the latter only minimizes the single point of greatest disagreement. This best-of-50 sensor placement set was then used to calculate the MAE' and β' for use with the single objective optimization problem in Equation (10).

Certain constraints were implemented in the code to ensure the GA progressed efficiently. The number of gene mutations per offspring was based on a shifted half-normal distribution, such that the probability of a one-gene mutated offspring is 0.5 and a 10-gene mutated offspring is 0.03 (3σ). Mutated genes are selected from all available genes, excluding the genes present in the parent (i.e. the parent cannot mutate back into itself). The probability of selecting a certain gene from the learning gene pool is based on that gene's relative selection weight. Selection weights were bounded to ensure that no sensor location would become overly dominant or drop out. The lower bound was set to 0.1, while the upper bound was set to 4. These bounds were selected to keep low-information genes available for selection and reward high-information genes, without allowing them to diverge to infinity. No constraints were enforced between individual offspring.

All GA iterations for parameter testing were run 10 times (the number of repeated GA runs $n_s = 10$) and terminated after 100 generations. The Student's t-distribution with $\nu = n_s - 1$ degrees of freedom was used to obtain an estimate of the true (population) mean from the sample

mean. Specifically, the 95% confidence interval for the true mean was developed based on the t-distribution to show with a degree of certainty where the true mean lies.

The proposed adaptive GA with learning gene pool easily lends itself to running in parallel code configurations as each offspring can be calculated independently. Code was developed using a series of Python codes, in combination with MATLAB's Parallel Computing Toolbox. Computations were performed using individual nodes on a high-performance computing cluster (HPC). Each node consisted of two 2.2 GHz 4-Core AMD Opteron 2354 with 8 GB of RAM. Algorithm speed was found to depend almost exclusively on the offspring population size. On average, a population size of 50 took 18.1 seconds per generation. The final sensor placement results were calculated in 26 hours running on 36 nodes.

Results of Experimental Validation

This section presents the results from the parameter studies used for the development of a final mutation-based GA configuration. Thereafter, the selected parameters are used to obtain an optimized sensor placement for the experimental HDSN.

Parametric study

First, the selection weights parameter is studied in relation to the GA's generational results. Tests were performed using a sample population of 50 with the code repeated over 10 runs to obtain a representative response. A reference case was obtained by solving a GA without a learning gene pool (selection weight = 0). The mean value of the 10 individual runs is shown in Figure 5(a). Through comparisons with the adaptive GAs of selection weights of 1% and 10%, it can be observed that the adaptive GAs with learning gene pool converge to a local minimum faster than the GA without a learning gene pool.

The effects of changing selection weights on the GA's fit after 100 generations are presented in Figure 5(b). The sample mean (i.e., a point estimate of the true mean) and the 95% confidence interval for the true mean are presented as a solid red and a dashed blue line, respectively. Small increases in selection weights for weights under ($< 1\%$) have a large effect on the GA's 100 generation results. However, the benefit of an increasing learning gene pool weights greatly diminishes for selection weights greater than 1%. For the remainder of the tests, a gene pool learning weight of 10% was used due to it being a typical response when compared to other weights $< 1\%$.

Next, the effect of population size on the adaptive GA with learning gene pool is studied. Again, each population size was tested over 100 generations and 10 runs with the mean of the 100th generation for population sizes ranging from 1-100 presented in Figure 6. The analysis shows that an increase in trial population size has a positive result on the GA's fitting ability, as expected. A greater improvement is seen for unit population increases up to 20 than for unit population increases after 20. Results presented here agree with the use of a population size of 50 as selected earlier. Thus, the population size of 50 is kept constant for all of the additional tests.

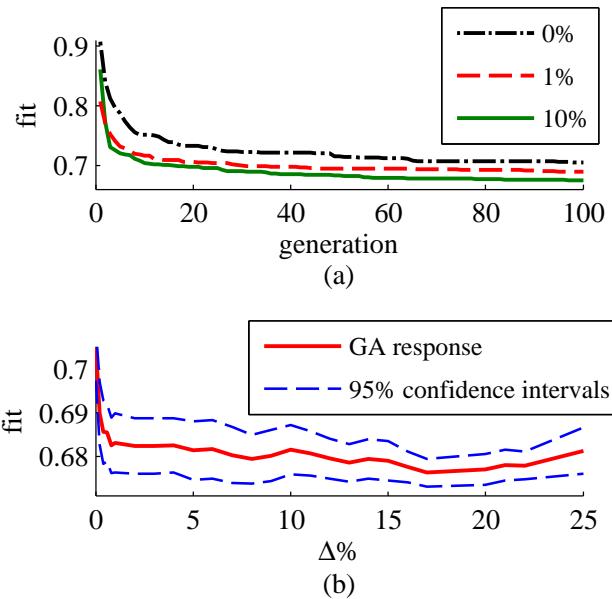


Figure 5. Effects of $\Delta\%$ on GA fit: (a) fit vs generation; and (b) fit after 100 generations vs $\Delta\%$.

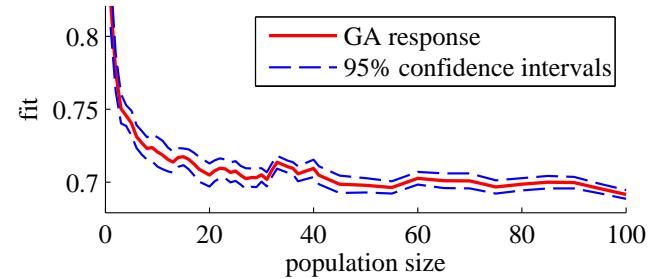


Figure 6. Effect of offspring population size on GA performance.

The concept of using multiple elites (parents) from each generation through the selection of the top k parents ($k = 1\dots 4$) was explored. After selecting the top k parents, the next generation was mutated from these with an equal number of mutations per parent. Any remaining offspring were applied to the leading parent to maintain a total population size of 50. Results showed no benefit to the introduction of multiple elites into the GA, therefore these results are omitted from the GAs formulation.

Lastly, a study of optimization objective function presented in Equation 10 is performed. Results presented in Figure 7 show that the proposed objective function is capable of developing a \mathbf{P} that accounts for potential type I and type II errors. For the experimental HDSN presented here, and considering type I and type II errors to be of equal importance, results demonstrate that $\alpha = 0.5$ provides an acceptable sensor placement set \mathbf{P} . Furthermore, when compared with a single objective function based purely on MAE (i.e. $\alpha = 0$), the selected value of $\alpha = 0.5$ provides a 12.53% improvement in β , while only resulting in a 1.47% cost in MAE. β has a local minimum at $\alpha = 0.7$, this is a consequence of $\alpha > 0.7$ putting greater emphasis on fitting one point per generation over 100 generations. Optimum fitting of sensor locations for $\alpha > 0.7$ requires excessive generations as the problem is solved through reducing the

point of greatest disagreement one-at-a-time. In comparison, $\alpha < 0.7$ adds more weight to fitting all the points, therefore ensuring that any single point of disagreement is less of an outlier. Selection of an appropriate α depends on engineering judgment but is taken here as $\alpha = 0.5$ for the subsequent simulations.

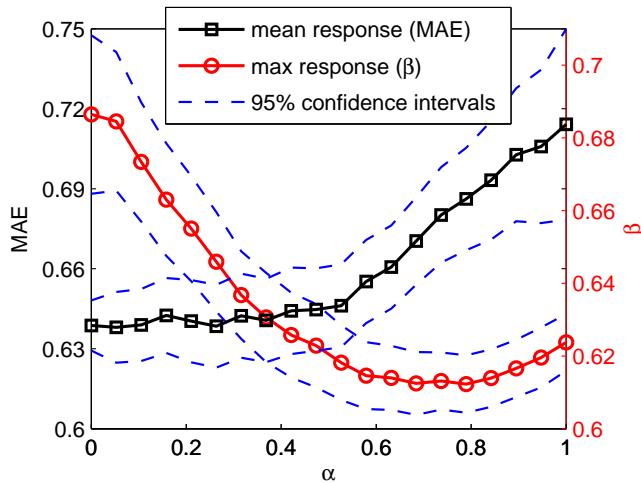


Figure 7. Bi-optimization objective function results presented as a function of the scalarization factor α for a the single objective function where: $\alpha = 0$ seeks to minimize type I error (MAE); $\alpha = 1$ seeks to minimize type II error (β).

Optimal Sensor Locations

Sensor placement for RSGs within the experimental HDSN is performed using a selection weight ($\Delta\%$) of 10%, a scalarization factor (α) of 0.5, and a population size of 50. The GA was run 360 times for 500 generations with the generational improvements reported in Figure 8(a). The 95% confidence interval for the true mean was estimated using Student's t-distribution as before, presented here as a solid black (true mean) and a dashed blue line (95% confidence interval). The P with the best fit at the 500th generation is presented as the red line with filled circle markers. As expected, the sensor placement fit improves through the generations with a final minimum fit of 0.655, a 34.5% improvement from the best-of-50 starting condition. Figure 8(b) presents a histogram showing the distribution for the final P, as found by each of the 360 runs with the optimal P being located in the left-most bin. Figure 8(b) demonstrates that the proposed algorithm is capable of repeatedly converging to an optimum solution, without developing any substantial outliers.

The starting guess best-of-50 results for sensor locations is presented in Figure 9(a). The purely random selection procedure selected five gauges in the x -direction, and five gauges in the y -direction. A MAE of $36\mu\varepsilon$ was obtained across all six strain maps with a maximum difference, β , of $201\mu\varepsilon$. Optimal sensor locations selected through the adaptive GA with learning gene pool are presented in 9(b). After optimizing RSG sensor layout, the MAE was reduced to $23\mu\varepsilon$ while β reduced to $131\mu\varepsilon$. The adaptive GA with learning gene pool prioritized the placement of strain gauges in the x -direction. This can be attributed to ε_x being the dominant strain in the test configuration under study (a

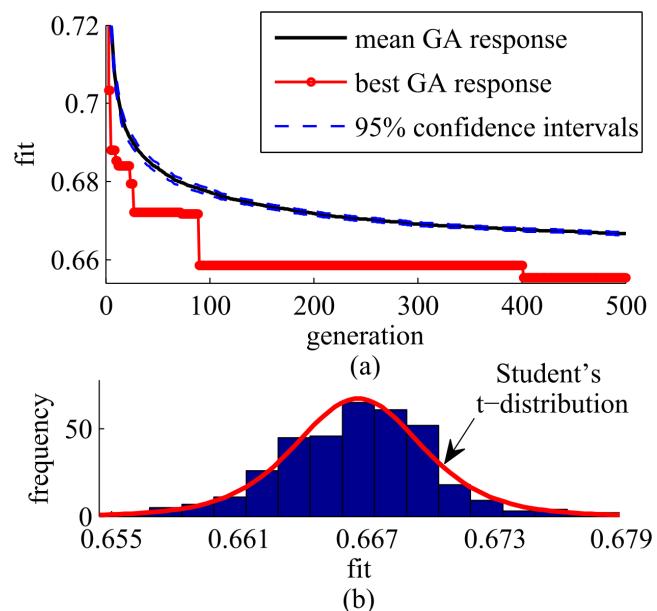


Figure 8. Results for obtaining the final set of sensor locations: a) generational results for adaptive GA with learning gene pool used for sensor placement; b) histogram showing the sensor results evenly distributed about the mean and compared to a Student's t-distribution.

dominant bending direction). Strain map reconstruction with the optimized RSG locations provided a 35% improvement in the HDSN's MAE and β (due to $\alpha = 0.5$) over the best-of-50 starting condition. The improved strain maps are considered rich enough to enable a good decomposition of the additive strain measured by the SECs. Note that weighted factors could be introduced in the objective function if, for instance, a higher degree of fit on ε_y would be required. The current sensor placement results are limited to the three loading cases presented here. Sensor placement for an extended loading case library and the effect of dynamic loading cases are left to future work.

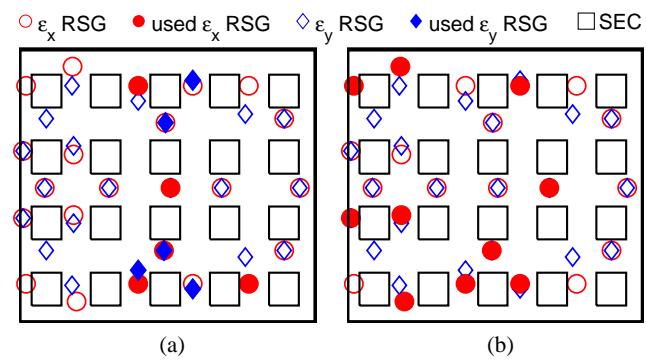


Figure 9. Optimized Sensor placement: (a) sensor placement for best of 50 random placements; and (b) sensor placement obtained through adaptive GA with learning gene pool.

Conclusion

This work presented a multi-objective optimization problem to reduce the occurrence of type I and type II errors in an SHM system, presented a case study of an adaptive

mutation-based GA with learning gene pool for placement of sensors within an HDSN and deployed an HDSN utilizing flexible electronics with optimally placed RSGs for the enforcement of boundary conditions. The effort presented here expands on the development of a low-cost sensing skin for the monitoring of large-scale structural components, including wind turbine blades. A novel sensor termed soft elastomeric capacitors (SEC) is combined with a mature technology, resistive strain gauges (RSGs), to form a hybrid dense sensor network (HDSN) capable of large-surface monitoring where the SEC provides low-cost additive in-place strain measurements over the entire system and the resistive strain gauges (RSG) are used for the enforcement of boundary conditions at key locations. When combined with a previously developed strain decomposition technique, uni-directional strain maps can be obtained, therefore, allowing the HDSN to act as a sensing skin capable of monitoring local uni-directional changes in strain over a global area.

An optimum sensor placement (OSP) for finding the key boundary condition locations for the deployment of RSGs within a grid of SECs was investigated with the intention to limit the number of RSGs used within the HDSN. A multi-objective optimization problem to reduce the occurrence of type I and type II errors in structural health monitoring (SHM) and prognostics and health management (PHM) was defined. The multi-objective optimization problem was formulated as a single objective optimization problem by linear scalarization. The objective problem was solved through an adaptive GA with learning gene pool for the placement of RSG sensors within the HDSN. The adaptive GA gene pool was updated every generation to reflect the quantity of information individual genes added to offspring.

Experimental validation demonstrated the adaptive GA's capability to efficiently place RSG sensors within an HDSN with consideration of predetermined loading cases. The efficient placement of RSGs sensors enables the deployment of large arrays of SECs over a large surface with the integration of a minimal number of RSGs. This will allow the monitoring of strain maps over large structural components, which information could be used to detect, localize, and quantify damage, or to create high fidelity models to enhance our understanding of certain structural behaviors. Such models can be particularly helpful in the development of PHM models and condition-based maintenance scheduling.

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